

A Review on Positive Semi Definite System on Vibration

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ABSTRACT

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In mechanical system dynamics, an eigenvalue with zero frequency signifies a rigid body motion mode. You are in this situation when you consider a system but do not apply the boundary conditions/constraints. For an object, a natural frequency can be one or more. The number of degrees of freedom in the system determines this. A system with one degree of freedom has a natural frequency of one. In a system with two degrees of freedom, there are two natural frequencies. Rigid-body modes are defined by zero natural frequencies in some dynamic systems. Some conceivable mode forms in zero-frequency systems may not entail any deformation. Rigid body modes are what they're termed. The associated frequencies are all zero. A wide range of applications are looking in to watch.

Keywords: Damped & Undamped system, Mode shape, Millidegree Freedom system

I. INTRODUCTION

These occur when the framework as a whole may move as a rigid body and vibrate. Semi-unequivocal frames are what they're called. They're also known as degenerate or illogical rigid body structures

$$[K-\omega^2m]x=0$$

The scenario mentioned here is one approach of expressing a problem with eigenvalues or brand esteem. The accompanying dislodging vectors express the opposing states of the vibrating system known as eigenvectors or mode shapes, while the quantities are the eigenvalues or trademark values exhibiting the square of the freevibration 2 frequencies. Under

specific conditions, every point in a framework could perform symphonies during free vibrations.

Because vibration at any of the two regular frequencies and abundance are coupled in a specific way, the design is known as normalmode or head modeof vibration. As a result, a two-level opportunity system has two common vibration mechanisms that compare two natural frequencies.

Dunkerley's condition is an old technique for reducing the primary recurrence of a multi-degree-of-freedom vibration framework. This strategy is really useful and important. As part of this technique, a series of circumstances were advanced; for example, in their book, Iablonskii et al. proposed a few

comparable conditions that were more accurate, can result in the upper and lower bounds of crucial recurrence, and can result in the second request of main recurrence. Sheng Shanding et al. synthesised Dunkerley's scenario into a unified framework, Yao Zuoqi reasoned two novel and easy hypothesised equations on normal frequencies, and Yan Shichaosynthesised DunkerleySouthwell's recipe for the structure-establishment framework. The Dunkerley criterion and its alternatives cannot be applied directly in some semidefinite instances.

Its dynamical lattice hasn't existed since then (p s-d framework). The designers developed yet another succinct method for making the p s-d framework's mass grid and solidness network nonsingular, which provides a vantage point for summarising the Dunkerley's condition for the p s-d framework. In light of this strategy, this research advanced the relating technique and condition.

II. SEMI-DEFINITE MDOF SYSTEMS, BOUNDARY CONDITIONS AND RIGID BODY MODES

Boundary conditions and their influence on mechanical vibration quality are two of the most essential topics covered in this course. What are boundary conditions, exactly? Take a look at the two-degree-of-freedom design in Figure and notice the two sets of springs and dampers. One set couples the two latencies (i.e., the two DOFs), while the other sets vibrates the two DOFs in a similar overall region. In this case, the spring and damper to ground at the left of DOF 1 structure the framework's limit state. The surface beneath the two DOFs is obviously a limit condition, but it isn't really fascinating in this case because the wheels are frictionless and the surface isn't particularly interesting

Positivedefinite if(Quadraticform) >0

Positivesemi-definite if(Quadratic form) ≥ 0

Negativedefiniteif(Quadraticform) <0

Because stiff body movements are common when systems vibrate, unbending body modes are critical in logical and exploratory vibrations. Train passenger vehicles, for example, can move along the track as rigid bodies to transport passengers from one spot to another, but they can also vibrate when energy is transmitted between the vehicles. To portray the train's total movements, the two forms of movement are required. The train can store the same amount of potential energy in the springs/joints between the vehicles in one location as it can in any other location along the track in terms of potential energy. Turning frameworks are the most well-known real use of rigidbody modes.

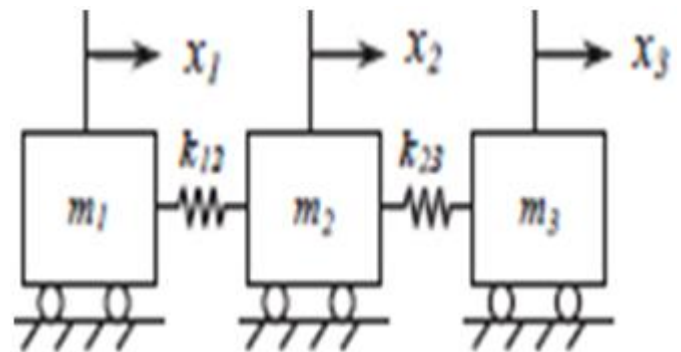


Fig. 3 DOF

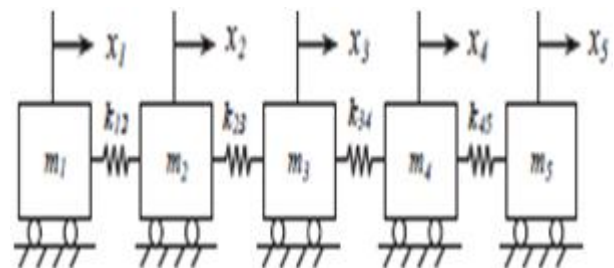


Fig. multi DOF

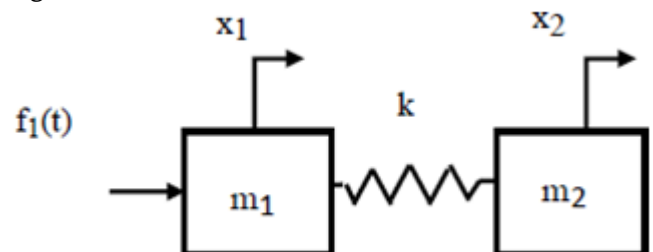


Fig. forced system

Translational quantity	Rotational quantity
Linear displacement x	Angular displacement α
Force F	Torque M
Spring constant k	Spring constant k_r
Damping constant c	Damping constant c_r
Mass m	Moment of inertia I
Spring law $F = k(x_1 - x_2)$	Spring law $M = k_r(\alpha_1 - \alpha_2)$
Damping law $F = c(\dot{x}_1 - \dot{x}_2)$	Damping law $M = c_r(\dot{\alpha}_1 - \dot{\alpha}_2)$
Inertia law $F = m\ddot{x}$	Inertia law $M = I\ddot{\alpha}$

Table .translatory and rotational quantity

The system shown below is a semi-definite system, meaning that one of its natural frequencies will be zero. For the following parameters, $M = 1000$ kg, $m = 400$ kg and $k = 10,000$ N/m, find the non-zero natural frequency.

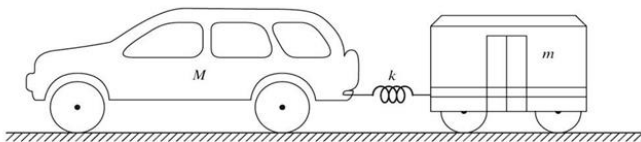


Fig. A semi definite system example

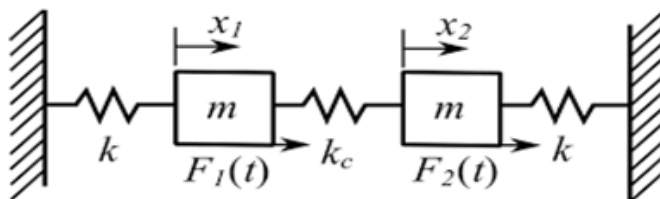


Fig. A Semi definite system example

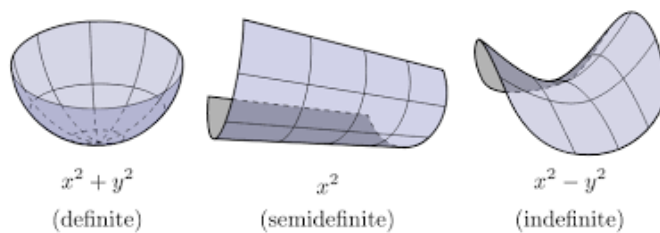


Fig. system of semi definite

In MDOF systems, a natural state is a shape configuration that the system adopts during motion. Furthermore, rather of simply one natural state, an MDOF system has a finite number of natural modes of vibration. Depending on the initial parameters or external driving stimuli, the system can vibrate in any of these modes or a combination of them. Each mode has a natural frequency that is unique to it. There are

as many natural frequencies as there are natural modes.

As a result, while the structure of a natural mode is unique, its amplitude is not. Even for systems with hundreds of DOFs, computers and mathematical calculation software now allow the assessment of all (or some) eigenvalues and their related eigenvectors in real time, using a single (simple) input. Important orthogonality requirements are met by the eigenvectors (natural modes).

	Mode 1	Mode 2
Mode shapes	$\psi_{1x} = 0$ $\psi_{1y} = 1$	$\psi_{2x} = 2x/a$ $\psi_{2y} = -(2y/b)$
Length of mode shapes, $L^2 = \int_V (\psi_x^2 + \psi_y^2) dV$	$L_1^2 = 1$	$L_2^2 = (1/3)(1 + (b^2/a^2))$
Modal mass, $m = \int_V \rho (\psi_x^2 + \psi_y^2) dV$	$m_1 = M$	$m_2 = (M/3)(1 + (b^2/a^2))$

Fig. mode shape for systems

	Mode 1	Mode 2
Mode shapes	$\psi_1 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$	$\psi_2 = \begin{bmatrix} -1 \\ 1 \end{bmatrix}$
Mass matrix M	$\begin{bmatrix} (M/4) + (J/a^2) & (M/4) - (J/a^2) \\ (M/4) - (J/a^2) & (M/4) + (J/a^2) \end{bmatrix}$	
Volume matrix V	$\begin{bmatrix} (V/4) + (V/12)(1 + (b^2/a^2)) & (V/4) - (V/12)(1 + (b^2/a^2)) \\ (V/4) - (V/12)(1 + (b^2/a^2)) & (V/4) + (V/12)(1 + (b^2/a^2)) \end{bmatrix}$	
Length of mode shapes, $L^2 = (1/V)\psi^T V \psi$	$L_1^2 = 1$	$L_2^2 = (1/3)(1 + (b^2/a^2))$
Modal mass, $m = \psi^T M \psi$	$m_1 = M$	$m_2 = (M/3)(1 + (b^2/a^2))$

Fig mode shape for systems

III. RESONANCE FREQUENCIES

When a system is subjected to forced, steady-state vibration, the peak values of its displacement, velocity, and acceleration response occur at slightly different forcing frequencies. Because a resonance frequency is defined as the frequency for which the response is at its maximum, a basic system has three resonance frequencies if defined broadly. Any of the resonance frequencies diverge from the natural frequency. The relationships between the various resonance

frequencies Natural frequencies that have been damped and those that have not been damped are
 Displacement resonance frequency: $\omega_n(1-2\zeta^2)^{1/2}$
 Velocity resonance frequency: ω_n
 Acceleration resonance frequency: $\omega_n/(1-2\zeta^2)^{1/2}$
 Damped natural frequency: $\omega_n(1-\zeta^2)^{1/2}$
 For the degree of damping usually embodied in physical systems, the difference among the three resonance frequencies is negligible

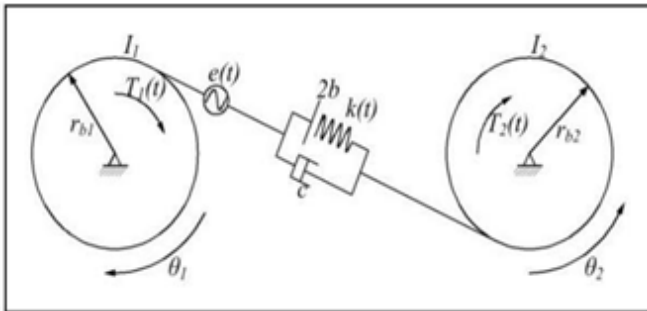


Fig. 1 DOF

The one level of opportunity paradigm is communicated in this way via the overall framework. Two mobility circumstances, namely two levels of opportunity and a semi-clear framework, can be used to create this paradigm. It is widely acknowledged that a single differential condition can be generated by conducting various operations on the two related conditions while managing just the vibration movement of the framework and not the rigid movement. As a result, in the literature, gear models that fit this definition are frequently referred to as one level of opportunity. As the mass of the framework is expanded, an unchecked natural occurrence of a single level of opportunity framework. As the mass of the framework increases, its usual recurrence decreases. The natural frequency of a human standing body is around 7.5 Hz, while the frequency of a seating posture in the cab is around 4–6 Hz.

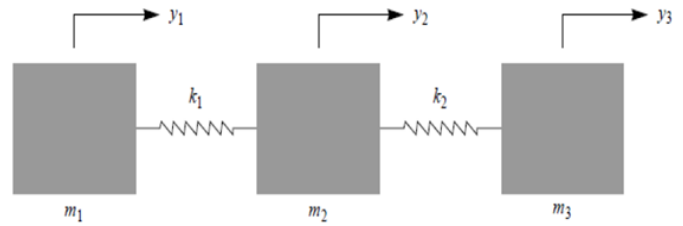


Fig . semi definite system

IV. CONCLUSIONS

This study investigated how to estimate the fundamental frequency of an undamped linear p s-d system and developed a general estimate equation comparable to Dunkerley's. The following are some of the inferences that can be drawn:

- (1) Dunkerley's equation can be applied to a linear p s-d system using the authors' method.
- (2) Equation can be used to estimate the fundamental frequency of a linear p s-d system, which is comparable to Dunkerley's equation.
- (3) A positive definite system's and a positive semidefinite system's fundamental frequencies can both be defined by their basic subsystems.
- (4) When the complete system may move as a rigid body while also vibrating, this occurs

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